EXPERIMENTAL VALIDATION OF EFFECT OF EQUIVALENCE RATIO ON DETONATION CHARACTERISTICS OF PROPANE/OXYGEN MIXTURES

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Abstract:
Experimental studies were carried out for using Propane as fuel for Pulse Detonation Engine application. In the present study Detonation Characteristics of Propane & Oxygen mixture at various equivalence ratios were presented. In these experiments Propane and Oxygen under regulated pressures were injected into a Detonation Tube from the head end using unlike impinging doublet injector. The fuel and oxidizer were allowed to mix and fill the tube. Subsequently, the mixture was ignited using a spark plug positioned close to the head end of the tube. The pressures generated due to the combustion of the mixtures were captured using five high frequency pressure transducers which were spaced 100mm apart on the detonation tube. Apart from these pressures, velocities of the combustion wave were computed using ‘time of flight’ method. These tests were done for different equivalence ratios varying from 0.8 to 1.6 by varying the feeding pressure of Propane. In the present study the performance of the combustion wave at different locations and effect of equivalence ratios on detonation characteristics were presented. In addition effect of presence of obstacles in the flow path i.e., Shchelkin spirals were also studied in reducing the Deflagration to Detonation Transition (DDT) distance.

Index Terms: Pulse Detonation, Propane, Injector, Equivalence Ration, Shchelkin Spiral, DDT.

I. INTRODUCTION

The need for faster flight, keeping fuel efficiency has propelled researcher’s inventive thinking into realms beyond imagination. Since the days of the Wright brothers, aircraft propulsion has come a long way. The invention of the gas turbine, and decades of research on it, has made the gas turbine a very effective source of power for air transportation, with very high fuel efficiency. The introduction of ramjet engines propelled airplanes to break the sound barrier with ease and became the main force for all the tactical missile applications. The latest in propulsion is the scramjet engine, where the design of a ramjet was improved to reduce losses from the shock waves made possible the historic X-43A hypersonic flight in March 2004.

An advanced propulsion system that is being researched is the Pulse Detonation Engine. This system has the ability to take-off without any auxiliary propulsion system from low to high mach and to cross the hypersonic barrier with highly fuel efficient manner.

Pulse detonation engines (PDEs) have emerged as potential devices to better utilize the chemical energy content of reactive fuel/air mixtures. One of the main advantages of PDEs is that detonations create less entropy when they combust a fuel/air mixture than conventional constant pressure combustion processes such as those used in current gas turbines, resulting in a more
efficient thermodynamic cycle. Establishing whether PDEs can achieve higher operating efficiency than conventional propulsion systems (i.e. gas turbines, ramjets, etc) is the focus of many research groups around the world.

II. OBJECTIVE

A. Pulse Detonation Engine

A detonation is a supersonic combustion wave that typically propagates at a few thousand meters per second relative to an unburned fuel/air mixture. Detonation is a much more energetic phenomenon than deflagration and produces higher pressures. A detonation wave compresses a fluid, increasing its pressure and density, in addition to increasing its temperature. Detonations can be approximated as supersonic shock waves that initiate and closely coupled to a thin flame front or combustion region. Due to the high speed nature of a detonation wave, detonation closely approximates a constant volume combustion process as compared to a constant pressure of Brayton cycle.

Pulse detonation engines (PDEs) have received considerable attention over the past three decades. These devices use detonation waves that propagate through a premixed fuel-air mixture and produce large chamber pressures and, thereby, thrust.

PDEs offer the potential for high performance because the rapid detonation process results in constant volume combustion with very high operating frequencies and combustor chamber pressures. PDEs are predicted to be very efficient and offer good thrust characteristics from the low subsonic to the high supersonic flight regimes. PDEs also have the potential to operate at very high energy densities, allowing the use of simple and compact combustor designs.

B. Basics of Pulse Detonation Engine (PDE)

The basic PDE has a very simple structure, as seen in Fig.1, consisting of a constant area tube, with valves to control the supply of fuel and oxidizer, an ignition system, and a nozzle for accelerating the flow if the engine is to be applied for propulsion. A practical PDE may also have one or more devices to bring about deflagration to detonation transition (DDT), such as a Shchelkin spiral. The PDE cycle has four stages, namely fill, combustion, blow down (exhaust) and purge. The four stages are presented in Fig.2.

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Fig.1 Schematic of Basic Pulse Detonation engine with valves at inlet and nozzle at exit
The PDE combustion chamber is filled with fuel and oxidizer during the fill stage. When the fuel-oxidizer mixture is filled to the required volume, the combustion stage commences when a spark is fired to start ignition. A detonation wave is soon created that moves through the mixture and causes the pressure and temperature behind it to rapidly shoot up. The next stage is the blow down stage, when a series of rarefaction waves travel upstream into the combustion chamber and reflect off the end wall, causing the high pressure burnt gases to exit the combustion chamber at a high speed. This is then followed by the purge stage, when fresh air is blown through to clean and cool the tube before the fill stage starts again.

Fig.2. Pulse Detonation engine Cycle

C. Scope of the Present Paper

This paper describes the basic characteristics of gaseous detonations. A test setup was established to study the various factors influencing the detonation of gaseous fuel Propane with Oxygen. Experiments were conducted to study the effect of equivalence ratio on detonation characteristics like CJ pressures and velocities. In addition tests were conducted to study the DDT by using Shchelkin spirals with different blockage ratios (BR).

III. EXPERIMENTAL SETUP

A. PDE Tube Configuration & Test Setup

The experiments were carried out using single detonation tube. The test setup layout is shown in Fig.1. The total tube is made from 4 sections. First section which is 150mm in length is having provision for mounting the spark plug. A conventional doublet injector is designed for supplying the fuel and oxidizer in to the tube. Second section is 450mm in length. This section is having provision for inserting the DDT device i.e, Shchelkin spirals. Pressure transducer mounting points are provided at 100mm distance a part. Third and Fourth sections are of 200mm and 300mm in length with Pressure transducer mounting points.

Fig.3. Dia 25mm PDE Tube Configuration
B. Propellant Feed System and Ignition

The Propane and Oxygen are supplied to the PDE tube through electrically operated direct acting Solenoid Valves. To get the required equivalence ratio, upstream pressures are controlled by using Pressure Regulators. The mass flows are calibrated using pre calibrated orifices placed in the injector line. The following picture shows the injector configuration.

![Fig.5. Injector Configuration](image)

The solenoid valves used for flow control are directing type. They operate with 24V DC current. The response times of the valves are 15 msec. The solenoid valves are kept in on condition for 5 sec such that the tube is filled and command is issued to the spark plug. The following picture shows the details of Spark Plug unit.

![Fig.6. Spark Ignition System](image)

The spark ignition system works with AC power supply. It generates around 2J. When switched on it maintains the spark for a period of 0.8msec.

C. Instrumentation & Data Recording

High response transducers are used for pressure pickup. These pressure transducers are having
100K sampling rate. As the pressure peaks are of the order of micro second, these sensors will be able to pickup Von Newman spike pressures very accurately.

Fig. 7. Pressure Transducer

The date recording is dome through National Instruments data acquisition system. The system is capable of programming the events like Solenoid valves ON/OFF and Spark Plug ON. The exact timings also can be controlled to the order of one micro second.

IV. TEST RESULTS

Series of experiments were carried out using Propane as fuel and Oxygen as oxidiser. The equivalence ratio (ER) is varied from 0.8 to 1.6 in steps of 0.2. The pressures were recorded using 5 nos of pressure transducers. They are placed at 250mm, 350mm, 450mm, 550mm, 650mm from the injector plane. Based on the Pressure Transducer location we can find out at what distance the detonation is occurring.

A. Experiments without DDT (Shchelkin Spirals)

First set of experiments were carried out with propane and oxygen without any DDT enhancing devices. The following Fig. show the pressures recorded during the tests. The units of pressure are Kg/cm² (Ksc). Five runs were taken with ER value ranging from 0.8 to 1.6.
Fig. 9. ER 1.0 without DDT device

Fig. 10. ER 1.2 without DDT device

Fig. 11. ER 1.4 without DDT device
 Remarks on Tests without DDT

1. From the graphs it is evident that detonation is achieved.
2. With 0.8 Equivalence Ratio (ER) the peak pressures recorded are around 25 Ksc. The maximum pressure recorded in K5 PT which is located at 650mm from head end of injector, which means that the detonation distance is around 650mm which is very high.
3. With 1.0 Equivalence Ratio (ER) the peak pressures recorded are around 29 Ksc. The maximum pressure recorded in K5 PT which is located at 650mm which means that the detonation distance is around 650mm which is very high.
4. With 1.2 Equivalence Ratio (ER) the peak pressures recorded are around 33 Ksc. The maximum pressure recorded in K1 PT which is located at 250mm which means that the detonation distance is around 250mm which is close to the expected value from the literature.
5. With 1.4 Equivalence Ratio (ER) the peak pressures recorded are around 37 Ksc. The maximum pressure also recorded in K5 PT which is located at 650mm and the shock wave was not sustaining. The detonation was not continuing.
6. With 1.6 Equivalence Ratio (ER) the peak pressures recorded are around 9 Ksc. From the graph it is clear that there was no proper detonation action inside the tube.

B. Experiments with DDT (Shchelkin Spirals)

Second set of experiments were carried out with propane and oxygen with DDT enhancing devices. The Shchelkin Spiral is 50 mm in length and blockage ratio(BR) of 43%. The following Fig. show the pressures recorded during the tests. The units of pressure are Kg/cm². Five runs were taken with ER value ranging from 0.8 to 1.6.
Fig. 13. ER 0.8 with DDT 50mm Shchelkin Spiral

Fig. 14. ER 1.0 with DDT 50mm Shchelkin Spiral

Fig. 15. ER 1.2 with DDT 50mm Shchelkin Spiral
Remarks on Tests with DDT device

1. From the graphs it is evident that detonation is achieved.
2. With 0.8 Equivalence Ratio (ER) the peak pressures recorded are around 25 Ksc. The maximum pressure recorded in K5 PT similar to the tests without DDT which is located at 650mm which means that the detonation distance is around 650mm which is very high. No improvement is observed with placement of DDT device.
3. With 1.0 Equivalence Ratio (ER) the peak pressures recorded are around 27 Ksc against 25 Ksc in the test without DDT. The maximum pressure recorded in K5 PT similar to the tests without DDT which is located at 650mm which means that the detonation distance is around 650mm which is very high. Not much improvement is observed with placement of DDT device.
4. With 1.2 Equivalence Ratio (ER) the peak pressures recorded are around 27 Ksc against 33 Ksc in the test without DDT. The maximum pressure recorded in K5 PT similar to the tests without DDT which is located at 650mm which means that the detonation distance is around 650mm which is very high. There a deterioration observed in the detonation pressures. So placement of DDT device is not helping in any way in improving the detonation characteristics.
5. With 1.4 Equivalence Ratio (ER) the peak pressures recorded are around 27 Ksc against 37 Ksc in the test without DDT. The maximum pressure recorded in K4 PT which is located at 550mm
and the shock wave was not sustaining. The detonation shock wave was not continuing.

6. With 1.6 Equivalence Ratio (ER) no detonation was observed in the tube.

V. CONCLUSIONS

A series of detonation experiments were conducted using Propane+Oxygen using Dia. 25mm tube. From the experiments with varying Equivalence ratio it is clear that best detonation is achieved with 1.2 ER in minimum possible DDT distance. These experiments give clear data for designing the pre detonator for two stage PDE engine.

From the experiments with varying Equivalence ratio with DDT device no significant improvement was observed in obtaining higher CJ Pressures or in reducing the DDT run up distance.

For Propane+Oxygen mixture Detonation can be achieved with minimum ignition energy and within a short distance of 300mm from the injector face of the detonation tube. The experimental data was validated with the NASA CEA detonation code results for the same mixture. The data is in close match.

Work was initiated to study effect of detonation tube diameter, shape and length on detonation characteristics. Optimisation of detonation initiation energy is also a very critical parameter which required a detailed study.

REFERENCES


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